

# Analytical Approach to Multiband Filter Synthesis and Comparison to Other Approaches<sup>1</sup>

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**Abstract**—A novel analytical approach to the synthesis of multiband electrical filters is presented. This approach allows to obtain the lowest possible order filters for a wide class of specifications including ones with large number of pass- and stopbands and with narrow transition bands. Comparison of the new approach to direct optimization and composite approaches is provided.

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## 1. INTRODUCTION

Currently, multiband filters are widely used in analogue and digital technology. For example, in modern microwave and RF communication systems, filters with several passbands corresponding to various standards of wireless communications are often required. The development of filters with multiband specifications is a difficult engineering task, especially if one wants to simultaneously ensure both high performance of the component and its compact implementation. To the current moment, there are no fully satisfactory and universal solutions to this problem in the literature.

An obvious approach is the composite one: multiband filter is obtained by interconnecting several single-band filters. Its disadvantage lies in too large orders of the synthesized filters implying their too large weight and dimensions. This explains the interest in the development of other approaches that are ideologically more sophisticated, but allow one to obtain filters of smaller orders under the same specification. At the level of technical implementation, engineers employ methods of microwave filter synthesis based on the use of multimode resonators [1, 2], as well as methods based on the use of frequency transformations (e.g., [3, 4]). The complexity of these approaches grows rapidly with the number of bands and the order of the filter. Also, applicable specifications have significant limitations.

Finally, a common method of filter synthesis is the direct numerical optimization of magnitude response. Here by *optimal* we mean a filter having the smallest order among all physically feasible filters that meet the requirements of the given specification (or the mask). The latter consists of the following parameters: 1) boundary frequencies of all pass- and stopbands; 2) maximal acceptable ripple at passbands and 3) minimal acceptable attenuation at stopbands. These data determine the desired shape of the filter magnitude response and only indirectly affect its other characteristics like phase response, impulse response etc.

Methods of filter synthesis connected with direct numerical optimization usually use Remez-type algorithms (see [5–7].) Due to their principal inherent instability these methods have a limited

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applicability range: with computations in double precision, the number of filter passbands does not exceed three, as a rule, while the filter order does not exceed twenty.

The authors of the article have developed an analytical approach to the synthesis of optimal multiband filters, which can be applied to specifications with a total number of bands (currently) up to 23 and with orders up to 1000. The aim of the article is to compare the new approach to the synthesis of optimal multiband filters with the direct optimization method based on the Remez-type algorithm, and also to compare optimal filters with non-optimal composite filters obtained by the corresponding approach. Section 2 introduces the optimization problem underlying the synthesis of the optimal multiband filter. Section 3 contains a brief description of the new analytical approach to this problem. In Section 4 the recipes that we used to solve the same problem by direct optimization method are given. Section 5 describes the composite approach to the synthesis of non-optimal multiband filters. Section 6 contains the results of numerical experiments made for the comparison of these three approaches.

## 2. PROBLEM FORMULATION

The search for an optimal filter corresponding to a given specification can be reduced to the solution of a series of least deviation problems of the type given below. To this end, at each step the filter order is fixed and one has to maximize, e.g., the attenuation at stopbands with all other specification parameters fixed. Consider two following formulations present in the literature.

Let  $E$  be the set containing  $m$  disjoint intervals of the real axis (frequency ranges) divided into two parts, the passbands  $E_+$  and the stopbands  $E_-$ . The ideal transition function  $F$  is equal to  $+1$  on intervals of  $E_+$  and to  $-1$  on intervals of  $E_-$ .

**Problem 1.** Find a real rational function  $R_n$  of degree at most  $n$ , for which the deviation from the transition function  $F$  is minimal in the uniform norm on  $E$ :

$$\|R_n - F\|_{C(E)} := \max_{x \in E} |R_n(x) - F(x)| \rightarrow \min =: \mu. \quad (1)$$

**Problem 2.** Find a real rational function  $Q_n(x)$  of degree at most  $n$ , which will minimize the quantity  $\theta$  under the constraints

$$\min_{w \in E_-} |Q_n(w)| \geq \theta^{-1}, \quad \max_{w \in E_+} |Q_n(w)| \leq \theta. \quad (2)$$

It is easy to show that these problems are equivalent while their solutions differ by a linear fractional substitution, i.e.,  $Q_n = l \circ R_n$  where  $l$  is the linear fractional transformation and the quantities inverse to the minimal deviations are related by the Joukowski transformation,  $\mu^{-1} = (\theta + \theta^{-1})/2$ .

Note that the two given formulations of the rational approximation problem coincide in essence with the third and fourth Zolotarev's problems for the condenser  $(E_+, E_-)$  [8]. The problem is multi-extremal: the entire set of rational functions is divided into  $2^{m-2}$  disjoint classes [9, 10], in each of which the solution exists, is unique and has an equioscillation characterization (or equiripple property): there are  $2n + 2$  points on  $E$  in which the deviation value for the solution of degree  $n$  is attained with a successive change of sign [11].

Until recently, the exact analytical solution of this problem was known only for the case  $m = 2$  (for one passband and one stopband), which was found in 1870's by Chebyshev's pupil E. I. Zolotarev [12]. It was about half a century later that it was used by the German electrical engineer W. Cauer [13] to construct the transfer functions of the optimal high- or low-pass filters, called afterwards the Cauer-Zolotarev (elliptical) filters. To date, these filters are widely used in analogue and digital technology, while the method of magnitude response approximation according to Zolotarev-Cauer became classical.

## 3. NEW ANALYTICAL APPROACH

Approach to the problems (1), (2) proposed in this paper is based on explicit analytical formulas obtained in [14] and generalizing Zolotarev's solution to the case of  $m$  components of  $E$  where  $m$  exceeds two. This approach was used earlier by the first author for the optimization of the uniform norm of polynomials [15]; its idea is as follows. The solutions of the optimization problem are very specific since they have a large number of equioscillation points and therefore lie on a certain manifold of small dimension in the space of all rational functions. When solving problems of least deviation, it is reasonable to move from searching the whole space of rational functions of given degree to the search over this small-dimensional manifold.

Indeed, the solution of the least deviation problem of degree  $n$  has  $2n + 2$  equioscillation points on  $E$  [11], and every such point lying in the interior of  $E$  will necessarily be a critical point of the solution function which takes there a value from the set  $Q$  containing four elements:  $\pm 1 \pm \mu$  for the formulation (1) and  $\pm \theta, \pm \theta^{-1}$  for the formulation (2). In total the rational function of degree  $n$  has  $2n - 2$  critical points counted with multiplicities, therefore the solution of the considered least deviation problem satisfies the following definition with the small parameter  $g$ .

**Definition.** The rational function  $R(x)$  is called  $g$ -extremal with respect to the 4-element set of values  $Q$ , if all its critical points with the exception of  $g - 1$  ones are simple with their values in  $Q$ . The number of exceptional critical points is given by the formula

$$g - 1 = \sum_{x: R(x) \notin Q} \text{ord } dR(x) + \sum_{x: R(x) \in Q} \left[ \frac{1}{2} \text{ord } dR(x) \right], \quad (3)$$

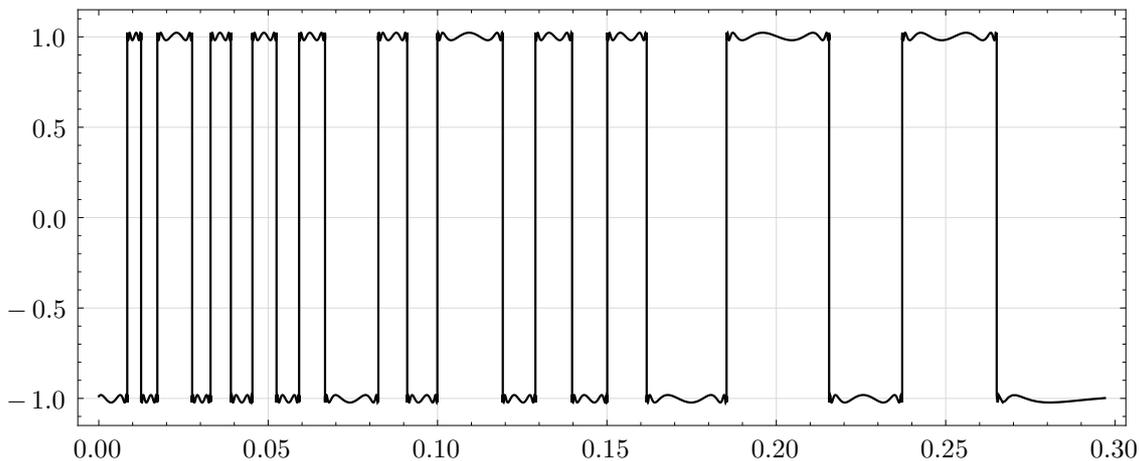
where the sum is taken over all points in the Riemann sphere;  $\text{ord } dR(x)$  is the order of the zero at the point  $x$  of the differential of the holomorphic map  $R: \mathbb{CP}^1 \rightarrow \mathbb{CP}^1$  (for instance, at simple poles of  $R(x)$  this quantity is equal to zero),  $[\cdot]$  is the integer part of a number.

Rational functions with the extremality number  $g$  possess the following effective low-parametric for small  $g$  and numerically stable representation [14] which generalizes the construction of Zolotarev's fraction:

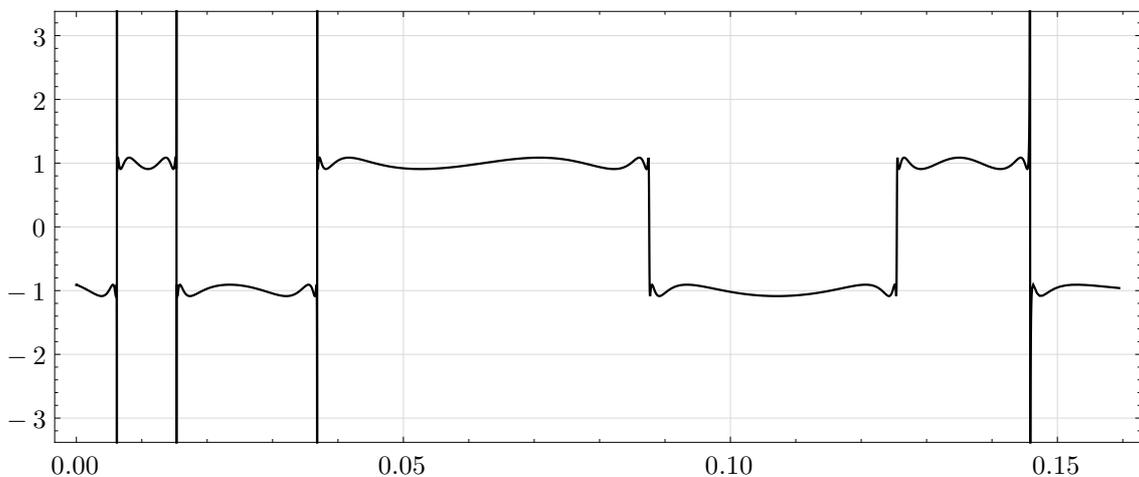
$$R(x) = \text{sn} \left( \int_e^x d\zeta + A(e) \mid \tau \right), \quad Q = \{\pm 1, \pm 1/k(\tau)\}, \quad (4)$$

where  $d\zeta$  is a holomorphic differential on a Riemann surface  $M$  of genus  $g$ , whose periods lie in the lattice of periods of elliptic sine, while the phase shift  $A(e)$  is also commensurable to this lattice. The surface  $M$  is determined by the rational function  $R(x)$  as the double covering of the Riemann sphere branched over the points  $e$ , where  $R(x)$  takes the values from the set  $Q$  with odd multiplicity. Emerging Riemann surface is not arbitrary, it is the so-called Calogero–Moser curve: it covers with due branching the torus defined by the set of distinguished values  $Q$ . By itself, the algebro-geometric representation (4) arises in the analysis of a functional equation of Pell–Abel type, which is satisfied by the rational function  $R(x)$  (for more details, see [14]).

The use of ansatz (4) for solving the optimization problem 1 or 2 implies finding all its parameters. First of all, it is necessary to determine the topological type of the real curve  $M$ , i.e. its genus and the number of real ovals, and also the location of the latter with respect to the components of the set  $E$  of filter bands. Assuming the alternation of the pass- and stop-bands, the genus  $g$  of the curve  $M$  is related to the number  $m$  of filter bands by the inequalities  $m - 1 \leq g \leq 2m - 3$ . After the discrete ansatz parameters are determined (currently, it requires a finite search or a qualified work to reduce it), it is possible to write a system of transcendental equations for the moduli of the pair (curve  $M$ , differential  $d\zeta$ ), whose solution is the required parameters of the ansatz (4), which allow the solution of the optimization problem to be reconstructed.



**Fig. 1.** Graph of the solution of the optimization problem (for a specification with  $m = 23$ )



**Fig. 2.** Graph of the solution of the optimization problem (for a specification with  $m = 7$ )

Representation of solutions in terms of conformal mappings of rectangular polygons (for instance, computable using theta functions [16]) is given in [14]. A more detailed exposition of the method based on the use of the explicit analytic formula (4) will be given in a separate article.

The employed parametrization of the extremal functions allows us to control the behavior of the solution in the transition bands of the filter, which corresponds to the selection of the class, and to solve the problem of the filter of the least degree for the given specification directly, without considering the chain of least deviation problems. The computational tools used to find extremal rational functions by the explicit analytic formula include the previously developed apparatus [14–18] for effective computations on Riemann surfaces, and allow one to compute in a stable way the solutions of degree  $n$  up to a thousand and more.

Using the new analytical approach, examples of solutions of optimization problem 1 were computed. A graph of the degree 654 solution function for a specification with the total number of bands  $m = 23$  is presented in Fig. 1. In Fig. 2 shown is the graph of a solution (for a specification with  $m = 7$ ), from a class that admits the presence of poles in the first, second, third and sixth transition bands.

## 4. DIRECT OPTIMIZATION

The solutions of the optimization problem can be computed approximately, e.g., using the Remez-type algorithms [9, 19, 20]. Starting point will be again the Akhiezer theorem [11]: the optimal rational function  $R(x) = \varphi(x)/\psi(x)$  of degree  $n$  must have at least  $2n + 2$  equioscillation points on  $E$ . Assume that we have an approximate fraction given, for instance, by position of zeros and poles or by coefficients of numerator and denominator in some polynomial basis. Assume also that we have the set of approximate equioscillation points which we denote by  $A$ . The algorithms in question consist in successive refinement of each of these two objects:

1. Having a set of points  $A \subset E$ , one can modify the fraction so that it will obey the equioscillation condition on the discrete set  $A$ ;
2. Having the fraction, one can modify the positions of points in order to increase the uniform error norm over  $A$ , or ensure oneself that this is impossible, i.e. the uniform error norm does not decrease if we restrict it from  $E$  to  $A$ .

Besides, an initial approximation is required, which is very important due to local convergence property of Remez-type algorithms. We describe briefly the recipes used for all mentioned steps.

*Choice of initial approximation.* We start by choosing the set  $A$ , namely, we use the  $1/(2n + 2)$ -quantiles of the equilibrium measure for the set  $E$ , which is computed using the numerical solution of the integral equation with the logarithmic kernel [21].

*Step 2 (refinement of  $A$  using the given fraction  $\varphi/\psi$ ).* First, we consider a wider set containing the endpoints of our  $m$  intervals and critical points of the error function  $\varphi(w)/\psi(w) - F(w)$  lying on  $E$ . Points corresponding to deviation less than the one obtained previously at Step 1, are discarded. The new set  $A$  must obey the rule of succession of signs and contain  $2n + 2$  points. The presence of more or less of them is corrected with the help of the previously introduced equilibrium measure, e.g., we discard the points corresponding to the smaller values of density of this measure. The search for critical points is carried out by the Brent method or, if the approximation is good enough, in a simpler way, using the Newton method.

*Step 1 (refinement of  $\varphi/\psi$  using the given set  $A$ ).* Unlike polynomial approximations, the equioscillation condition for the set  $A$  cannot be represented, to our knowledge, in the form of a linear system; the best formulation one can obtain is a generalized eigenvalue problem of the form

$$\begin{pmatrix} V_+ & -V_+ \\ V_- & V_- \end{pmatrix} \begin{pmatrix} \varphi \\ \psi \end{pmatrix} = \mu \begin{pmatrix} 0 & \Sigma_+ V_+ \\ 0 & \Sigma_- V_- \end{pmatrix} \begin{pmatrix} \varphi \\ \psi \end{pmatrix} \quad (5)$$

for the first formulation of the extremal problem, and of the form

$$\begin{pmatrix} V_- & 0 \\ 0 & \Sigma_+ V_+ \end{pmatrix} \begin{pmatrix} \varphi \\ \psi \end{pmatrix} = \theta \begin{pmatrix} 0 & \Sigma_- V_- \\ V_+ & 0 \end{pmatrix} \begin{pmatrix} \varphi \\ \psi \end{pmatrix} \quad (6)$$

for the second one (see §2). The latter problem can be found in [9]. In the equations (5), (6), the following notation is used:  $V_{\pm}$  – the Vandermonde matrix corresponding to the nodes of  $A$  which belong to  $E_{\pm}$ ;  $\Sigma_{\pm}$  – diagonal matrices with entries  $\pm 1$  fixed for every pass- or stop-band, corresponding to the nodes of  $A$ , which belong to  $E_{\pm}$ ;  $\varphi, \psi$  – vectors of numerator and denominator coefficients corresponding to the rational fraction;  $\mu, \theta$  – extremal alternating values. The presence of matrices  $\Sigma_{\pm}$  is due to the possible change of equioscillation signs in adjacent intervals.

As can be seen, the matrix problems (5), (6) are unsymmetric, and corresponding matrix pencils may turn out to be singular; even in the case of two intervals it may happen that standard mantissa computations are not sufficient for getting at least one decimal digit of coefficients of  $\varphi$  and  $\psi$  (let alone their roots). Besides, the search over all variants of equioscillation signs in adjacent intervals means an exponential in  $m$  complexity.

A certain advantage over the eigenvalue problems belongs to the reduction of the problem (1) formulated for a given set  $A$ , to a linear programming problem. Here also emerges an exponential in  $m$  search related to the choice of the sign of denominator of the fraction for each interval. Here is the problem: minimize the quantity  $t > 0$  under the nonlinear constraints

$$|\varphi(x) - \psi(x)F(x)| \leq t|\psi(x)|, \quad x \in A, \quad j = 1, \dots, m,$$

which turn to linear ones if we fix the sign of  $\psi(x)$  on each interval. Good results for this problem are shown by the primal-dual interior point method [22].

Linear parametrization of numerators and denominators of the fraction limits the stability of Remez-type algorithms [19] substantially. The maximal degree of the solution  $R$  obtained by such methods working in double precision depends on configuration of the set  $E$  but does not exceed  $n = 20$ .

## 5. COMPOSITE APPROACH

Composite approach is not connected with the formulated optimization problem and implies obtaining a (non-optimal) multiband filter as a result of combining several single-band filters. Architecturally, this can be implemented, for instance, by parallel connection of bandpass filters, each of which maintains one band of the given multiband specification, or by cascade connection of bandpass and band-rejection filters.

Non-optimal filters obtained by composite approach hereinafter are referred to as composite filters. We used the following recipe for their construction: for each passband, the transfer function of the corresponding passband elliptical filter was computed, then the resulting functions were added. The parameters of elliptical filters were optimized by manual search to achieve the smallest possible order of the resulting multiband filter under the condition that its magnitude response fits into the corridor given by the specification.

## 6. EXAMPLES OF SYNTHESIS

Here we give examples of the results of design of digital multiband filters using three approaches: the new analytical approach, the direct optimization method, and the composite approach. The first two approaches are based on the optimization problem formulated above and give optimal filters (i.e., filters of the minimum possible order for a given specification). The latter approach consists in combining single-band elliptical filters and gives non-optimal multiband filters.

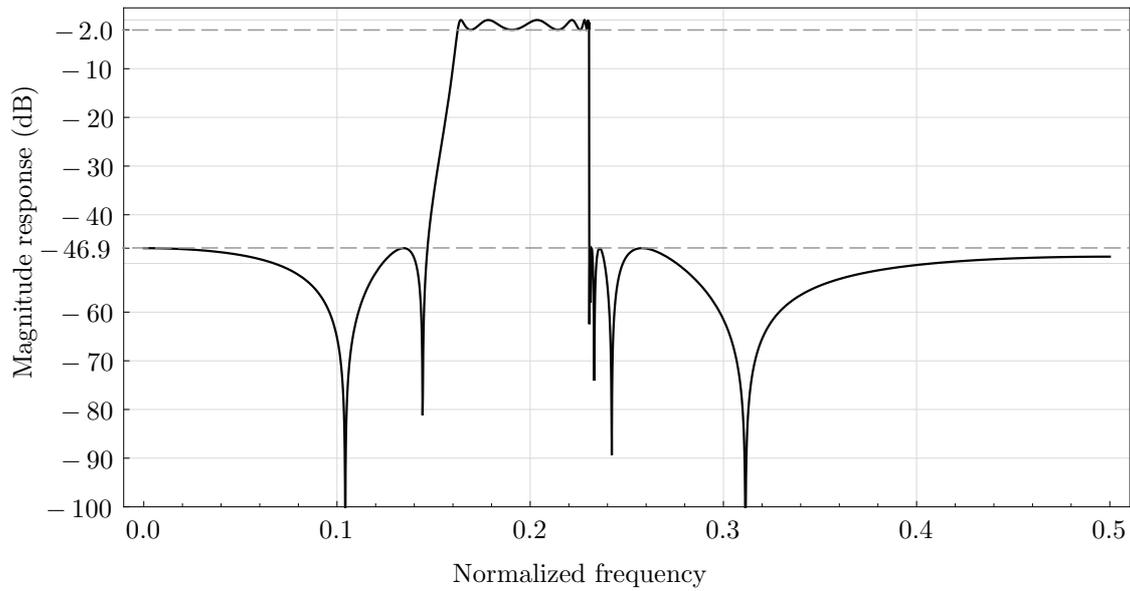
Optimal digital filters were obtained from optimal analogue ones by the standard (so-called bilinear) frequency transformation.

The direct optimization did not yield satisfactory results for any of the considered examples due to the complexity of the specifications. Its results are given for the first and second examples. The composite approach, as can be seen from the examples, yields filters with significantly higher orders in comparison with the optimal filters.

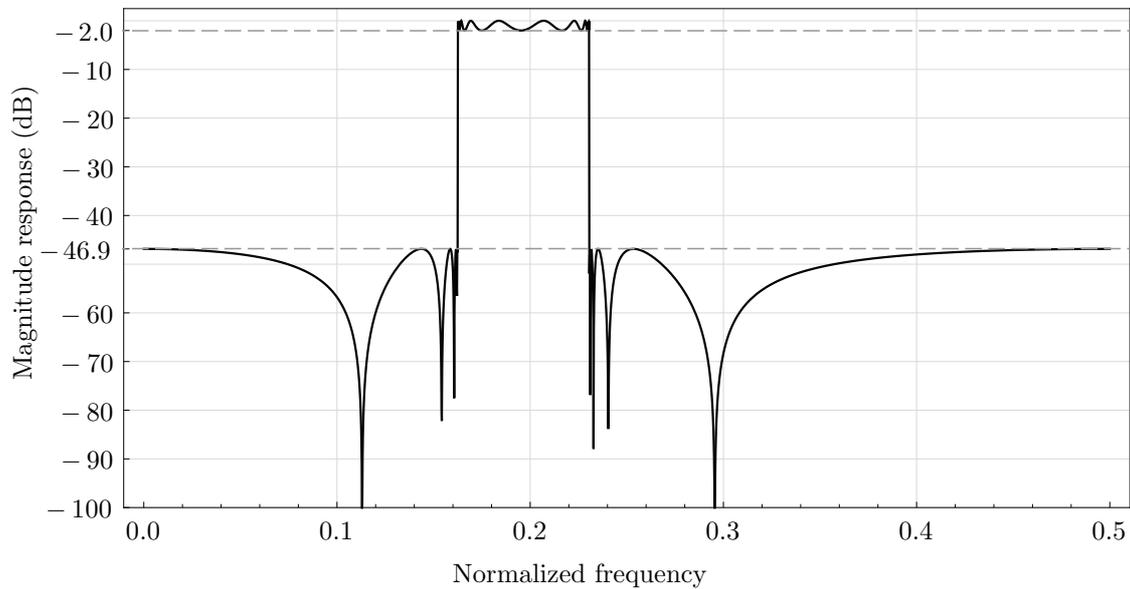
### 6.1. Single-band filter.

With the help of the new analytical approach, we constructed a single-band optimal filter of the 18th order with strongly asymmetrical widths of transition bands equal to 0.016 and  $2 \cdot 10^{-5}$ . The graph of its magnitude response is shown in Fig. 3.

The standard frequency transformation used in the synthesis of the passband elliptical filter from the low pass prototype cannot provide such a difference in the widths of the transition bands.



**Fig. 3.** Magnitude response of single-band optimal filter



**Fig. 4.** Magnitude response of single-band elliptical filter

So, the elliptical filter computed according to the same specification has a larger order, namely, 28. The graph of its magnitude response is presented in Fig. 4.

The results of the direct numerical optimization for that specification are given in Table 1. In computations using the Remez algorithm, the boundaries of the filter bands were given by specification, the passband ripple was fixed equal to  $-2$  dB, and the attenuation in the stopbands (the second column in the table) was determined from the order of the optimal filter obtained. The  $-46.9$  dB attenuation in the stopbands turned out to be unattainable for the direct optimization method due to the fact that even the computation of the filter of order 10 required quite a lot of time.

**Table 1.** Results of the direct numerical optimization for a single-band filter

3	-3.381	102
4	-4.227	154
5	-7.589	211
6	-10.612	308
8	-19.355	457
9	-22.378	652
10	-	> 1000
18	-46.9	?

**Table 2.** Results of the direct optimization for a dual-band filter

3	-5.342	151
4	-9.178	273
5	-12.649	351
6	-16.013	408
7	-19.215	594
8	-	> 1000
16	-40	?

### 6.2. Dual-band filter.

As an example of an optimal dual-band filter, a filter of the order 16 was constructed using the analytical approach, with a minimum attenuation at the stopbands equal to  $-40$  dB and a passband ripple equal to  $-2.6$  dB. The widths of the transition bands: 0.012, 0.012, 0.003, 0.008. The magnitude response graph is shown in Fig. 5.

The composite filter constructed according to the same specification is of the order 23. The graph of its magnitude response is presented in Fig. 6.

The results of the direct optimization for that specification are given in Table 2. In computations the boundaries of the filter bands were given by specification, the passband ripple was fixed equal to  $-2$  dB, and the attenuation in the stopbands (the second column in the table) was determined from the order of the optimal filter obtained. In this case the Remez-type algorithm turned out to be unapplicable for the search of optimal filters starting already from the order eight which means that the optimal filter of the order 16 obtained by the analytical approach cannot be found by the direct optimization method.

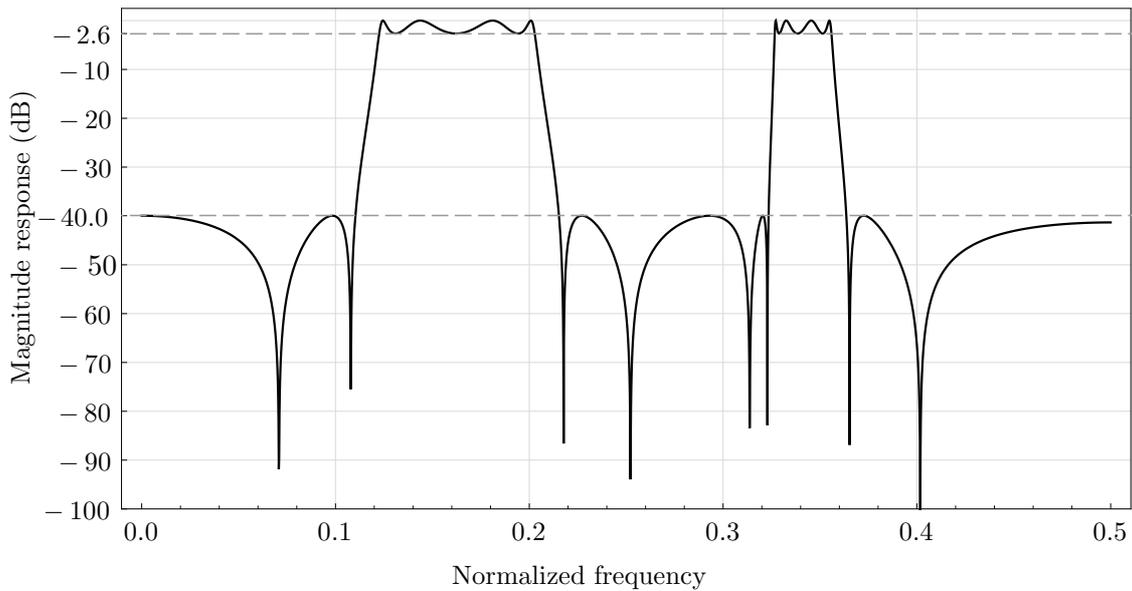
### 6.3. Four-band filter.

With the help of the analytical approach, we synthesized a four-band optimal filter of the order 36 with a minimum attenuation at the stopbands equal to  $-42.8$  dB, ripple at the passbands equal to  $-2.0$  dB, and with widths of the transition bands from 0.002 to 0.005. The magnitude response graph of the obtained filter is shown in Fig. 7.

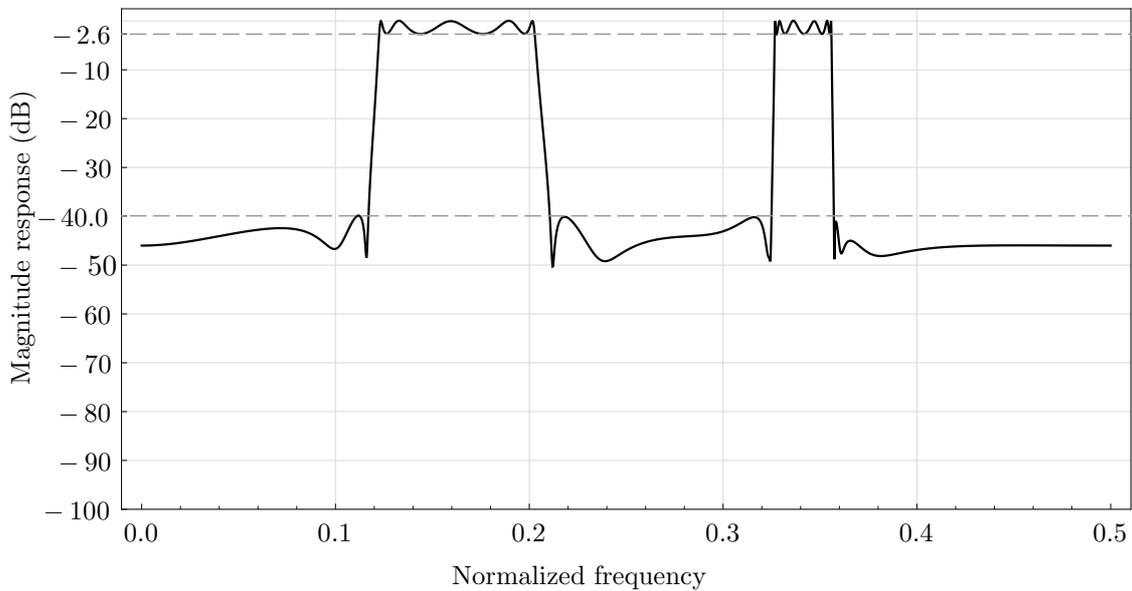
The composite filter constructed according to the same specification is of the order 55. The graph of its magnitude response is presented in Fig. 8.

### 6.4. Five-band filter.

For the five-band specification, the optimal filter of the order 76 was computed with a minimum magnitude response attenuation at the stopbands equal to  $-50$  dB, a passband ripple equal to



**Fig. 5.** Magnitude response of a dual-band optimal filter



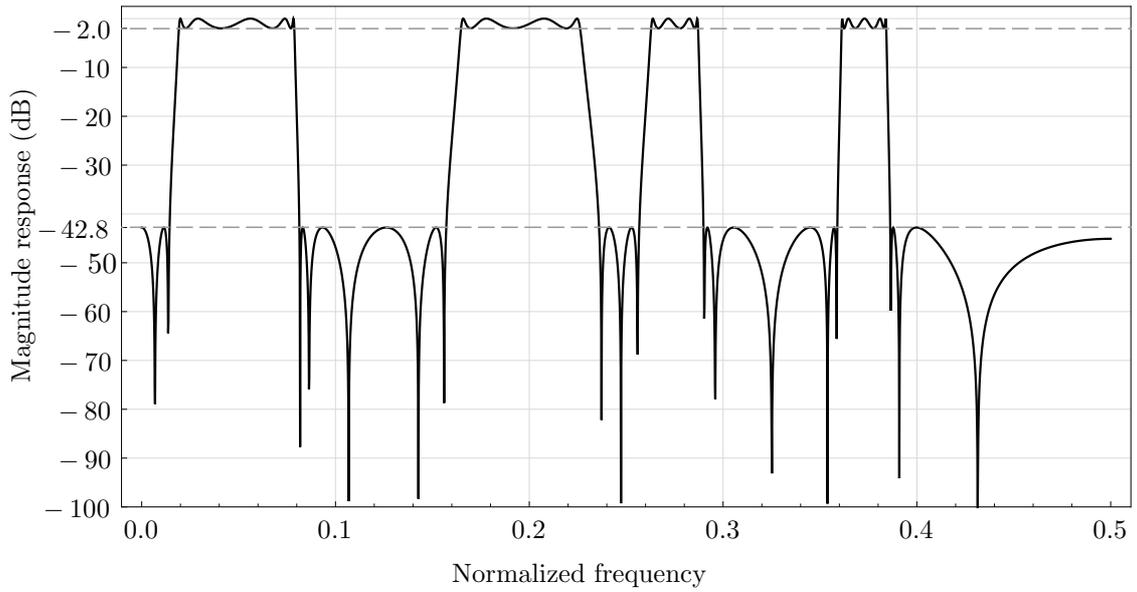
**Fig. 6.** Magnitude response of a dual-band composite filter

-2.0 dB. The widths of the transition bands belong to the interval from 0.002 to 0.005. The magnitude response graph is shown in Fig. 9.

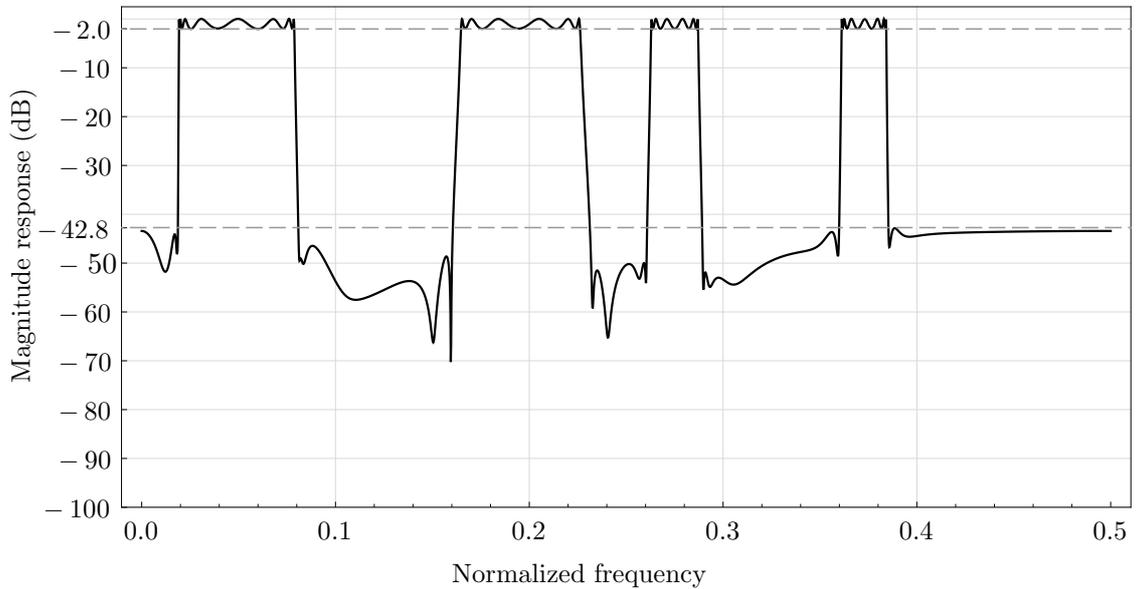
The composite filter constructed according to the same specification is of the order 121. The graph of its magnitude response is presented in Fig. 10.

### 6.5. Notch filter with two rejection bands.

The magnitude response graph of the optimal notch filter of the order 16 performing accurate cutting of two given frequencies is presented in Fig. 11. The fragment of the magnitude response containing the rejected frequencies is presented on a larger scale in Fig. 12.



**Fig. 7.** Magnitude response of a four-band optimal filter



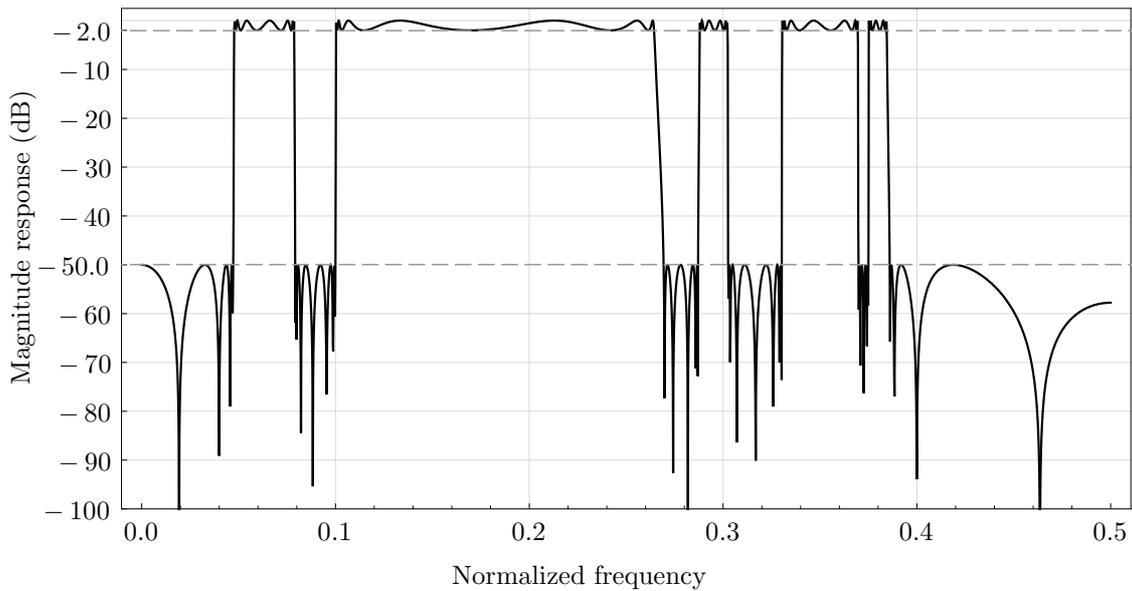
**Fig. 8.** Magnitude response of a four-band composite filter

The composite filter maintaining the same magnitude response approximation quality is of the order 62.

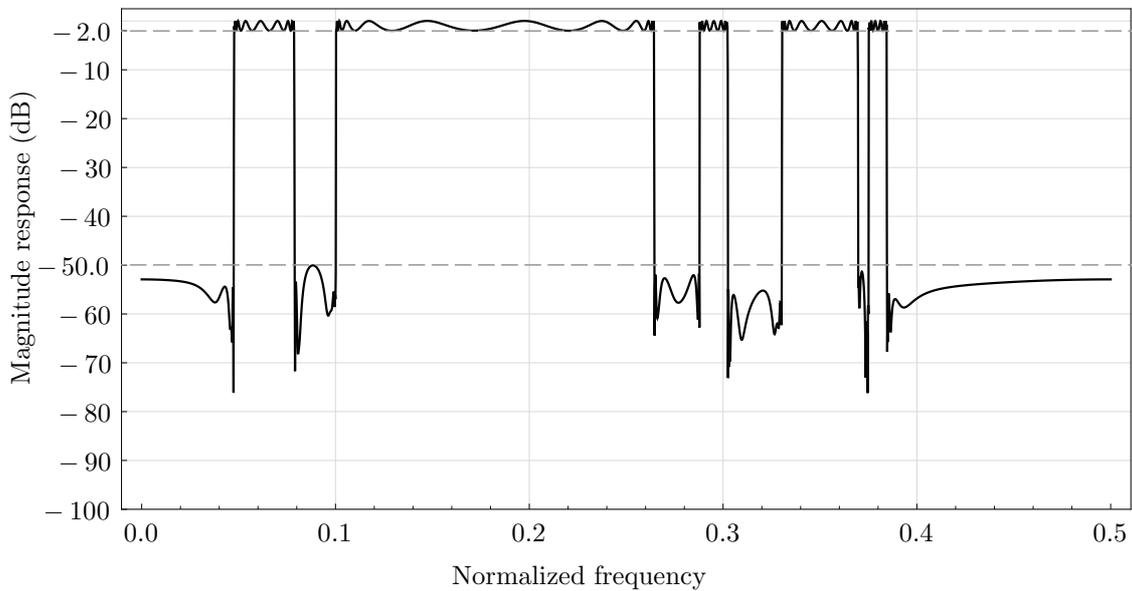
#### *6.6. Filter with two passbands critically close to each other.*

With the help of the analytical approach, we constructed the optimal filter of the order 24 with two passbands critically close to each other. The corresponding magnitude response graph is given in Fig. 13. Such filters can be used if it is required to extract a certain frequency range from the spectrum while rejecting one or several frequencies contained within that range.

The composite filter maintaining the same magnitude response approximation quality is of the order 59.



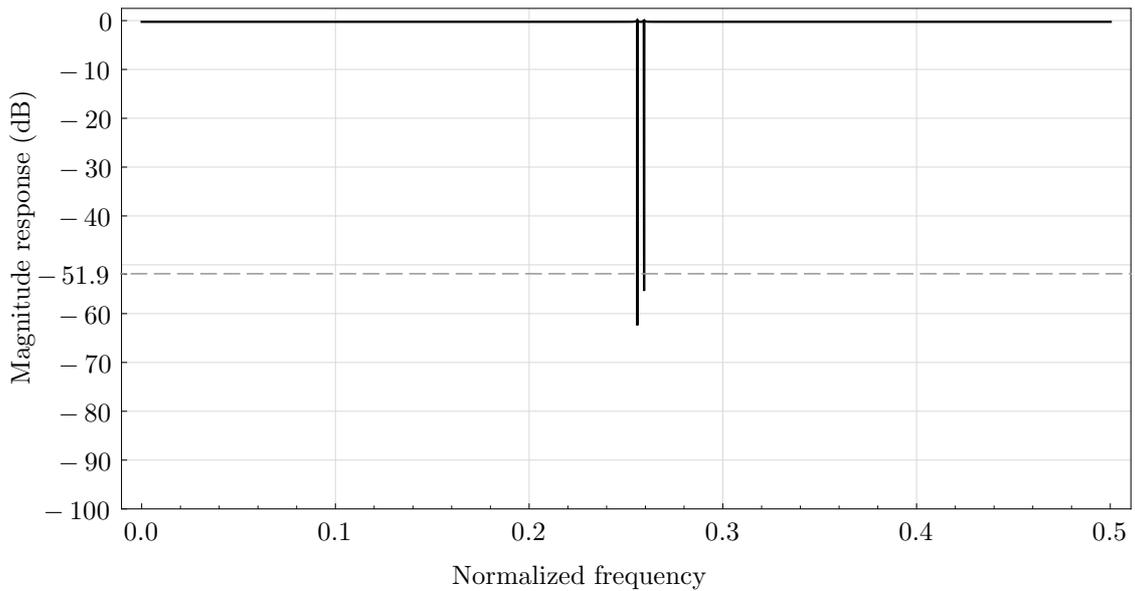
**Fig. 9.** Magnitude response of a four-band optimal filter



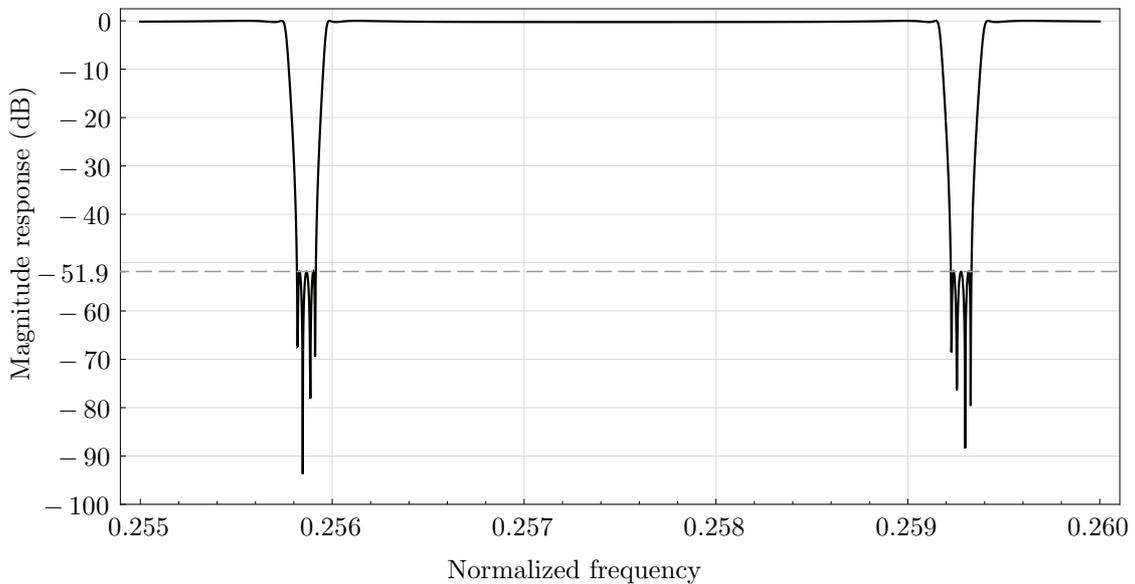
**Fig. 10.** Magnitude response of a four-band composite filter

## 7. CONCLUSION

The article gives a comparison of three approaches to the synthesis of multiband filters: the new analytical approach, the direct numerical optimization based on Remez method and semi-analytical composite approach. Today, the direct numerical optimization has probably the widest algorithmic support: there exist (and are being improved) mature packages for engineering computations. Unfortunately, the unavoidable instability of Remez-type algorithms does not allow to solve too complicated problems: in double precision arithmetic (15 decimal digits) the filter order does not attain 20, and the good approximation properties are unreachable in the case of complicated specifications, for instance, with the large number of pass- and stop-bands, narrow transition bands, critically close passbands. The composite approach consists in breaking up a complex problem

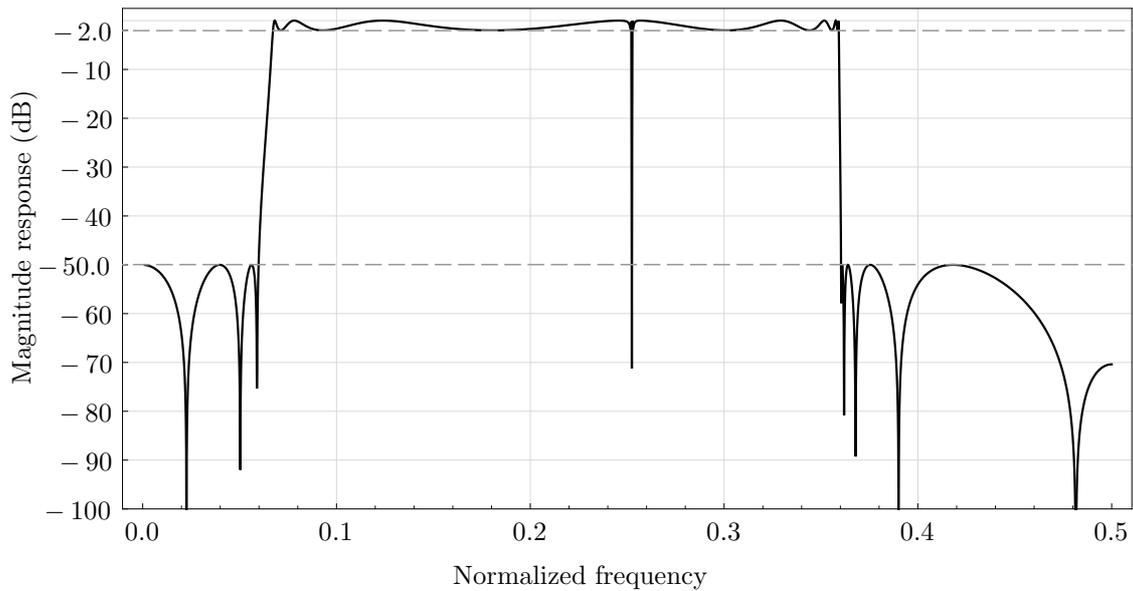


**Fig. 11.** Magnitude response of the optimal notch filter with two rejection bands

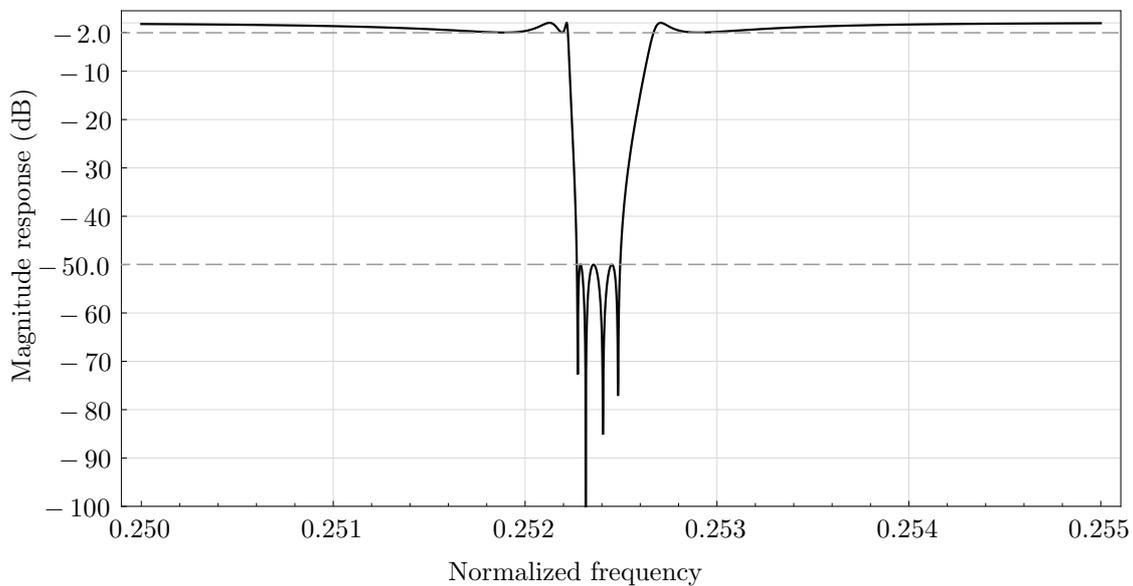


**Fig. 12.** Fragment of the magnitude response containing the rejected frequencies

into a series of simple ones and in their successive solving by using Zolotarev's fraction for the construction of the passband filter magnitude response. Its advantage is that in this way it is always possible to obtain an (ersatz) solution for a given specification. As a rule, it is far from being optimal: the order of composite filter can be several times greater than the order of optimal filter with the same specification. The situation gets worse with the increasing complexity of the filter specification. From our point of view, the most promising, as well as the least studied from the algorithmic aspect, is the analytical approach based on a complex mathematical apparatus. The authors intend to continue their research in this direction.



**Fig. 13.** Magnitude response of the optimal filter with two passbands critically close to each other



**Fig. 14.** Fragment of the magnitude response containing the rejected frequency

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